

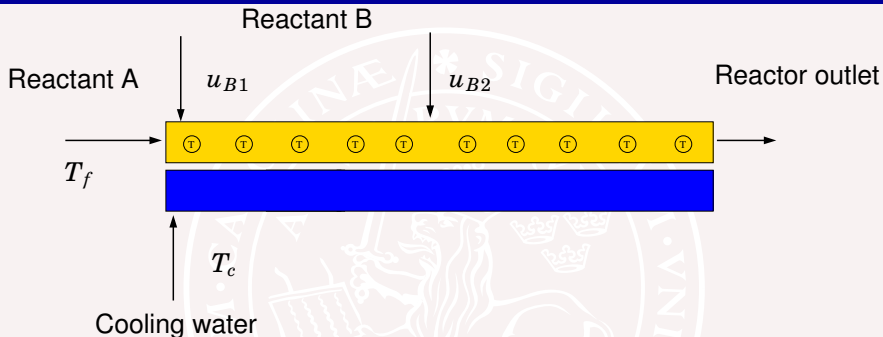


Dynamic optimization of a plate reactor start-up

**Staffan Haugwitz, Per Hagander and John Bagterp
Jørgensen**

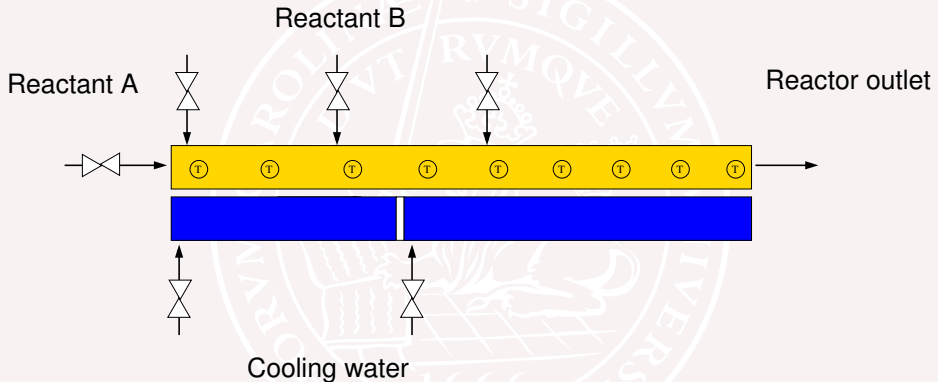
Lund-Lyngby-Ålborg-dagen 061101

Process configurations : 2 inj. / 1 cool zone

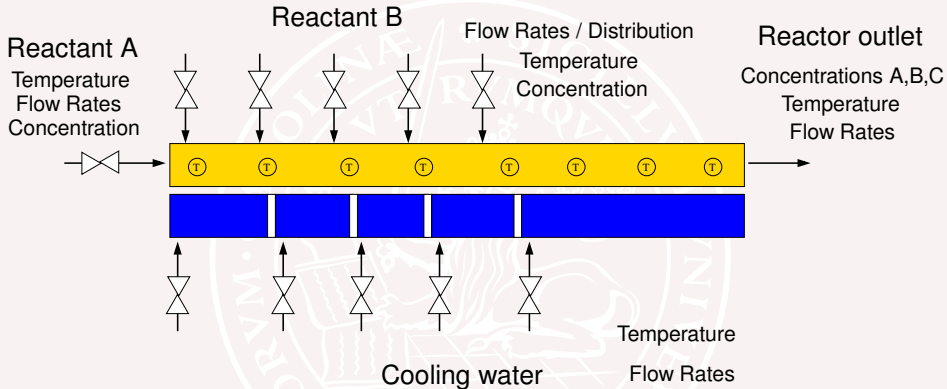


- Large flexibility in injection points and cooling zones.
- More actuators lead to better performance, but more expensive and complex process.
- Four control variables: $u_{T_{feed}}$, $u_{T_{cool}}$, u_{B1} and u_{B2}
- PDE model is discretized to a system of ODEs

Process configurations : 3 inj. / 2 cool zones

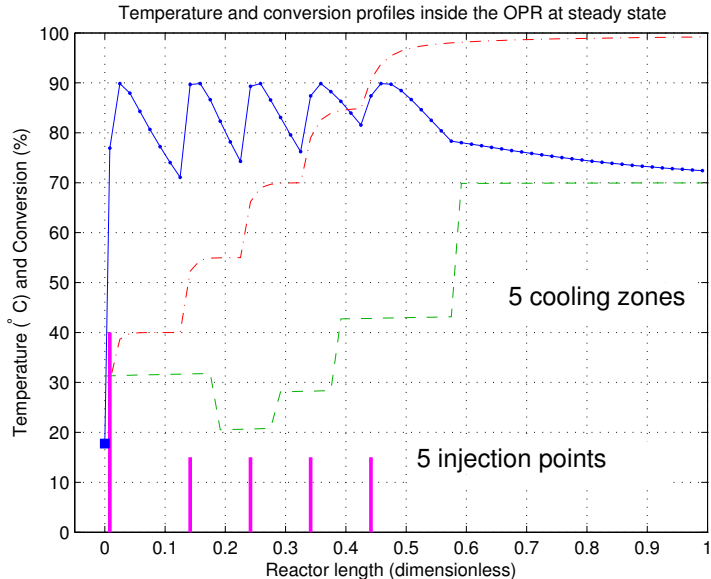


Process configurations : 5 inj. / 5 cool zone



Large flexibility: 18 input variables available for control !

Process design choices



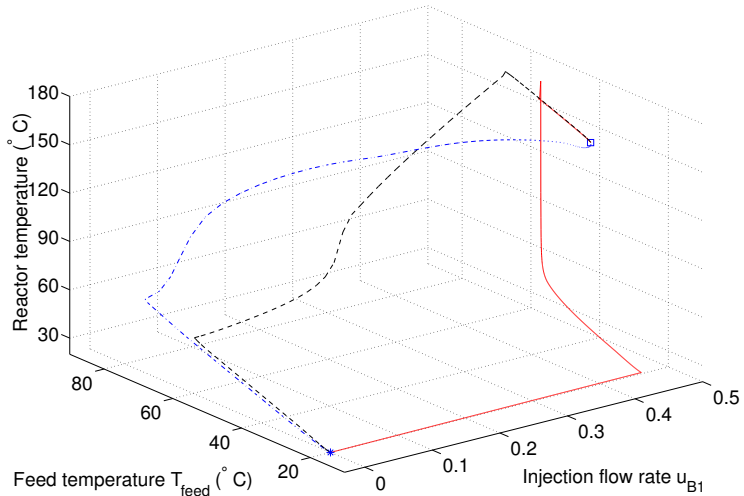
Start-up objectives & challenges

- Bring the process *safely* from initial cold state to optimal operating point with full heat release
- Minimize minimize off-spec product, amount of outflowing unreacted chemicals or minimize start-up time
- Highly nonlinear dynamics with multiple steady states
- Limiting actuator dynamics
- Process uncertainties

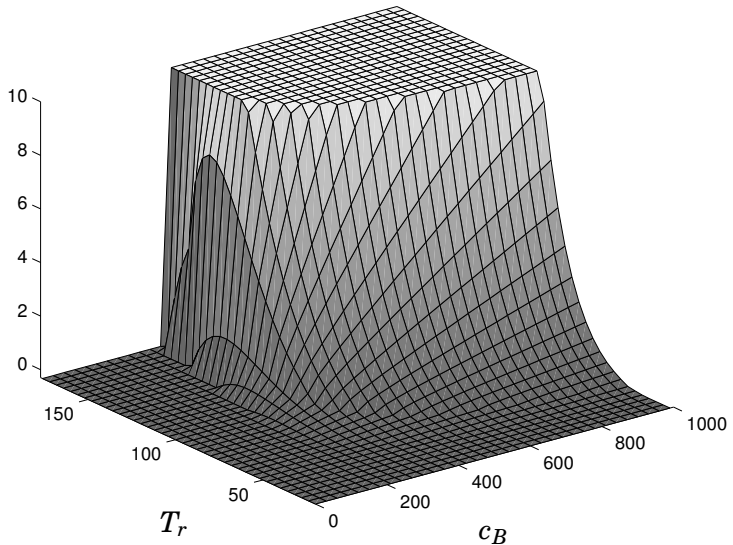
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Motivating examples



Motivating examples cont'd



Safety conditions for ignition and conversion

Avoid regions in the state-space, where there are fast and dangerous dynamics

- 1 The reactor temperature should be driven to a required initial temperature at which reactant B can be fed into the reactor safely
- 2 Before the next downstream injection starts, it is necessary to check that almost all reactants injected upstream has converted

Nonlinear Model Predictive Control

Components in the controller

- Nonlinear model is available, derived from first principles (120 states), PDEs discretized to a system of ODEs.
- Dynamic optimization by a single-shooting, using ESDIRK methods for integration and sensitivity computation
- Extended Kalman filter
- NMPC needed primarily for start-up, but also for optimization of productivity, finding operating points for parallel reactions...

Details of the NMPC implementation

Cost function

$$\phi = \underbrace{\int_{t_0}^{t_p} g(x(t), u(t), \bar{u}(t), r(t)) dt}_{=\phi_1} + \underbrace{\frac{1}{2} \sum_{k=0}^{N-1} \|\Delta u_k\|_{2,S}^2}_{=\phi_2} \quad (1)$$

where

$$\begin{aligned} g(x(t), u(t), \bar{u}(t), r(t)) = \\ \frac{1}{2} \|C_z x(t) - r(t)\|_{2,Q_z}^2 + \frac{1}{2} \|u(t) - \bar{u}(t)\|_{2,R}^2 \\ + \frac{1}{2} \|s(x(t))\|_{2,Q_{2s}}^2 + \|s(x(t))\|_{1,Q_{1s}} \end{aligned} \quad (2)$$

and $s(\cdot)$ is a soft constraint penalty function

Details of the NMPC implementation

Objective function

$$\psi = \psi(\{u_k\}_{k=0}^{N-1}) = \{\phi : \dot{x}(t) = f(x(t), u(t), d(t)), x(t_0) = x_0\} \quad (3)$$

The optimization problem is then

$$\min_{\{u_k\}_{k=0}^{N-1}} \psi = \psi(\{u_k\}_{k=0}^{N-1}) \quad (4)$$

- **Compute ψ by integrating forward, given guess on $\{u_k\}_{k=0}^{N-1}$**
- **Compute $\nabla_{u_k} \psi$ by integrating backwards**
- **Compute new control trajectories by solving NLP**

The Alfa Laval plate reactor

